

(Add)  $K, Y, \sigma, \mu$

P218 F01  
Lecture 18

①

## Tensors of Elasticity

### The Stress Tensor

Consider a small planar region  $\Delta x \Delta z$  passing through a point  $\vec{r}$ . What is the force of the material to the left of  $\vec{r}$  on the material to the right?

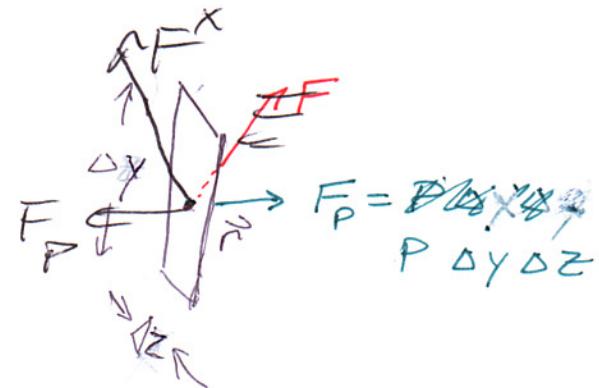
Proportional to  $\Delta y \Delta z$ : divide out

Define

$$\sigma_{i1} = F_i / \Delta y \Delta z$$

$$\boxed{\sum F_p} \quad \sigma_{i2} = F_i^y / \Delta z \Delta x$$

$$\boxed{F_p} \quad \sigma_{i3} = F_i^z / \Delta x \Delta y$$



Exercise: If the material is a fluid, at pressure  $P$ , what's the force?

$$\vec{F} = P \Delta y \Delta z \hat{x}$$

$$\frac{F_1}{\Delta y \Delta z} = \sigma_{i1} = P$$

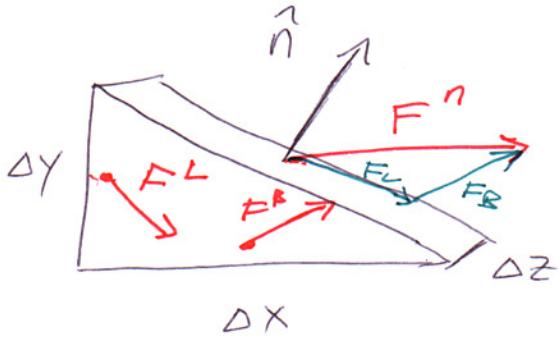
$$F_2 = F_3 = 0$$

$\sigma_{ij}$  = Stress Tensor

$$\frac{1}{3} \sigma_{ii} = (\sigma_{xx} + \sigma_{yy} + \sigma_{zz})/3 = \text{Pressure}$$

Fact  $\sigma_{ij} \hat{n}_i = \left( \frac{\text{Force}}{\text{Area}} \right) \text{ across surface perpendicular to } \hat{n}$

Proof in Two Dimensions:



$$\hat{n} = \frac{1}{\sqrt{\Delta x^2 + \Delta y^2}} \begin{pmatrix} \Delta y \\ \Delta x \end{pmatrix}$$

$$\vec{F}_i^L = \Delta y \Delta z \sigma_{i1}$$

$$\vec{F}_i^B = \Delta x \Delta z \sigma_{i2}$$

$$\frac{\vec{F}_i^n}{\text{Area}} = \sigma_{i1} \frac{\Delta y}{\sqrt{\Delta x^2 + \Delta y^2}} + \sigma_{i2} \frac{\Delta x}{\sqrt{\Delta x^2 + \Delta y^2}}$$

$$= \sigma_{i1} \hat{n}_1 + \sigma_{i2} \hat{n}_2 = \sigma_{ij} \hat{n}_j \quad \checkmark$$

Assume tiny triangle of material in equilibrium: force

$$\vec{F}_L + \vec{F}_B = \vec{F}_N$$

(As size  $\rightarrow 0$ , mass  $\rightarrow 0$ , acceleration finite  
 $\rightarrow$  net force = 0)

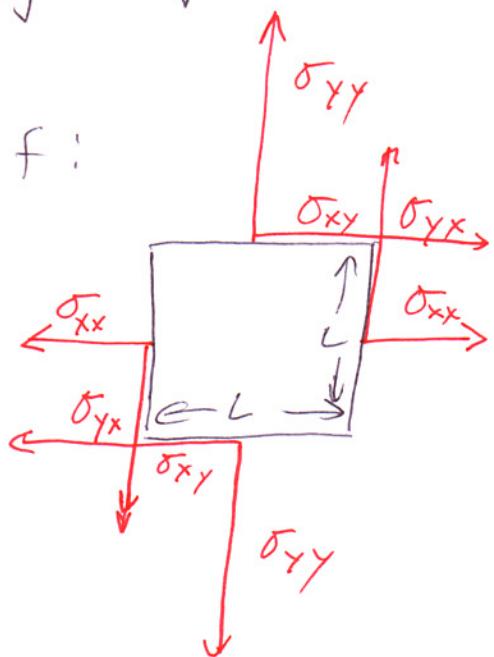
$$\vec{F}_i^n = \sigma_{i1} \Delta y \Delta z + \sigma_{i2} \Delta x \Delta z$$

$$\text{Area of Face} = \Delta z \sqrt{\Delta x^2 + \Delta y^2}$$

Fact

$$\sigma_{ij} = \sigma_{ji} \quad (\text{Stress is a symmetric tensor})$$

Proof:



Assume cube is in equilibrium

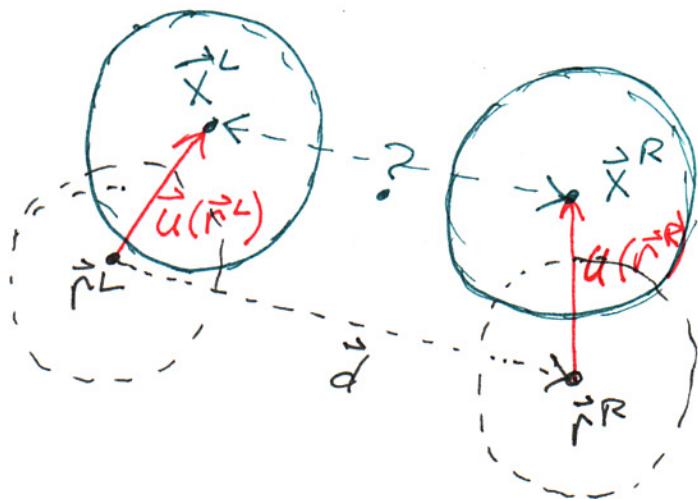
Total Force = 0 ✓

$$\begin{aligned} \text{Total Torque} \\ = (\sigma_{yx} - \sigma_{xy}) \cdot L = 0 \end{aligned}$$

$$\Rightarrow \sigma_{xy} = \sigma_{yx}$$

## The Strain Tensor

[Standard derivation in texts; this fancy one from Landau & Lifshitz Elastic Theory of Elasticity p.1]



Two atoms, undistorted positions  $\vec{r}^L, \vec{r}^R$ , distorted positions  $\vec{x}^L, \vec{x}^R$ . Displacement field

$$\vec{u}(\vec{r}) = \vec{x}(\vec{r}) - \vec{r}.$$

Original distance  
 $\vec{d}^2 = (\vec{r}^L \cdot \vec{r}^R)^2$  Final distance

Strain tensor tells how far the original distance vector  $\vec{d}$  will stretch.

$$\begin{aligned}
 (\vec{x}^R - \vec{x}^L)^2 &= [\vec{r}^R + \vec{u}(\vec{r}^R) - \vec{r}^L - \vec{u}(\vec{r}^L)]^2 \\
 &= [d_i + u_i(\vec{r}^L + \vec{d}) - \vec{u}_i(\vec{r}^L)]^2 \quad \text{Summation convention} \\
 &\approx [d_i + d_j \delta_j u_i]^2 \quad \vec{u}(\vec{x} + \vec{h}) - \vec{u}(\vec{x}) \approx (\vec{h} \cdot \vec{\nabla}) \vec{u} \\
 &= d_i^2 + 2 d_i d_j \delta_j u_i + d_j^2 u_i^2 \quad \text{true for vectors as well as functions}
 \end{aligned}$$

Old distance

$$d_i d_j \delta_j u_i = d_i d_j \delta_i u_j$$

$$= d_i d_j (\frac{\delta_i u_j + \delta_j u_i}{2})$$

$\uparrow$   
 Interchange dummy indices i and k

$$(\text{New distance})^2 - (\text{Old distance})^2$$

$$= 2 d_i d_j \left[ \frac{\partial_i u_j + \partial_j u_i}{2} + \frac{\partial_i u_k \partial_j u_k}{2} \right]$$

$$= 2 d_i d_j \varepsilon_{ij}$$

Strain tensor

$$\varepsilon_{ij} = \frac{1}{2} \left[ \underbrace{\partial_i u_j + \partial_j u_i}_{\text{Symmetrized Gradient}} + \partial_i u_k \partial_j u_k \right]$$

Geometric Nonlinearity

The geometric nonlinearity is usually ignored. Strains for most materials (not rubber) above 1% lead to permanent bending (plastic flow).

$$\varepsilon_{ij} \sim 0.01 \Rightarrow \partial_i u_k \partial_j u_k \sim 10^{-4}, \text{ ignore.}$$

Except: Rubber

Large rotations (wires,  
thin sheets,  
grain boundaries)

## The Tensor of Elasticity

Hooke's Law  $F = KX$ ,  $F/A = Y \frac{\Delta L}{L}$ , ...

Force  $\leftrightarrow$  Stress tensor  $\sigma_{ij}$

Stretch  $\leftrightarrow$  Strain tensor  $\epsilon_{kl}$

$$\sigma_{ij} = \underbrace{c_{ijkl}}_{\text{Elastic Tensor}} \epsilon_{kl}$$

- How many elastic constants for an anisotropic material?

-  $i, j, k, l \ 1, 2, 3 \Rightarrow 81$  at most.

$\epsilon_{kl} = \epsilon_{lk} \rightarrow (c_{ijlk} + c_{jilk})$  value irrelevant for  $\sigma$

$\rightarrow$  set  $c_{ijlk} = c_{jilk}$

$$c_{ijlk} = c_{jilk}$$

Six choices of  $\{c_{ij}\}$ , six choices of  $\{c_{kl}\}$

$\rightarrow 36$  at most.

Use formula for the energy, ~~Problem 7.6.2d~~

Problem 7.4.1  $\Rightarrow$  {21 possible independent elastic constants.}