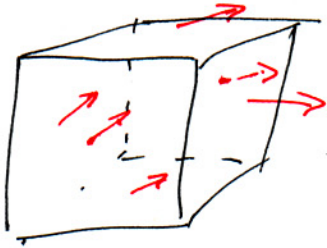


Forces

Net Force on a Small Cube!



$$F_i^o = \sum_{6 \text{ faces}} (\text{~~x~~ th component of force on face})$$

$$= [\sigma_{i1}(x+\Delta x) - \sigma_{i1}(x)] \Delta y \Delta z$$

$$+ [\sigma_{i2}(y+\Delta y) - \sigma_{i2}(y)] \Delta x \Delta z$$

$$+ [\sigma_{i3}(z+\Delta z) - \sigma_{i3}(z)] \Delta x \Delta y$$

$$F_i = \partial_j \sigma_{ij} dV$$

Newton's Law!

$$F = ma = m \frac{\partial \vec{u}}{\partial t}$$

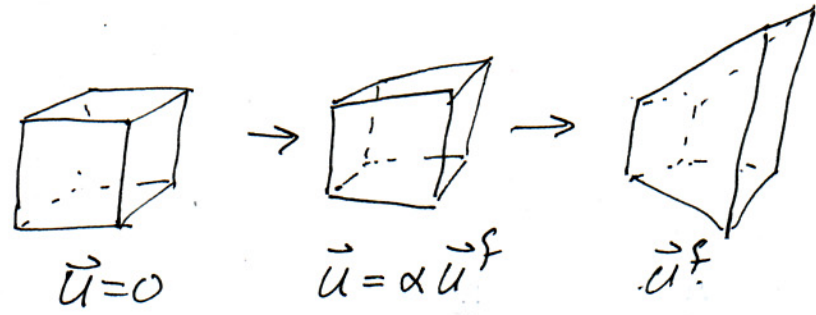
$$(\rho dV) \partial_0^2 u_i = \partial_j \sigma_{ij} dV$$

$$\rho \partial_0^2 u_i = \partial_j \sigma_{ij} = \partial_j (\epsilon_{ijkl} \epsilon_{kl})$$

$$[E\&H \text{ notation: } \rho_0 \frac{\partial \vec{p}}{\partial t^2} = \vec{\nabla} \cdot \underset{\substack{\text{w} \\ \text{Strain tensor}}}{\mathbf{F}}]$$

We'll return to this...

The Elastic Energy



Parameterize path from $\vec{u}=0$ to final $\vec{u}=\vec{u}^f$
linearly: $\vec{u}=\alpha\vec{u}^f$ $0 < \alpha < 1$.

Consider the work done by the body on the external world as $\vec{u} \rightarrow \vec{u} + \delta\vec{u} = \alpha\vec{u}^f + (\delta\alpha)\vec{u}^f$

Notice: this is minus the energy flow into the body.

The work done equals

$$\int \left(\frac{\text{Force}}{\text{volume}} \right) \cdot \delta\vec{u} \, dV = \int \underbrace{(\partial_j \sigma_{ij})}_{du} \cdot \underbrace{(\delta u_i)}_V \, dV$$

More fun with integration by parts!

$$u = \sigma_{ij} \quad dV = \partial_j (\delta u_i)$$

Assume $\sigma_{ij} \rightarrow 0$ far away, drop uv term

$$\begin{aligned} &= - \int \sigma_{ij} \partial_j (\delta u_i) \, dV \\ &= - \int \sigma_{ij} \partial_j u_i^f \, dV \, \delta\alpha \\ &= - \int \sigma_{ij} \left(\frac{1}{2} (\partial_j u_i^f + \partial_i u_j^f) \right) \, dV \, \delta\alpha \\ &= - \int \sigma_{ij} \epsilon_{ij}^f \, dV \, \delta\alpha \end{aligned}$$

$$\text{Now, } \sigma_{ij} = C_{ijkl} \epsilon_{kl} = C_{ijkl} \left(\frac{1}{2} (\partial_i u_j + \partial_j u_i) \right)$$

αu_j^f αu_i^f
 n_i n_j

$$= \alpha \sigma_{ij}^f \quad [\text{Hooke's law again}]$$

Minus Energy
Flow into
Body $x \rightarrow x + \delta x$

$$= - \int \sigma_{ij}^f \epsilon_{ij}^f dV \quad \alpha \delta x$$

Total Energy Stored
in Body

$$= \int \sigma_{ij}^f \epsilon_{ij}^f dV \int_0^{\alpha} \alpha d\alpha$$

$\underbrace{\hspace{10em}}_{\frac{1}{2}}$

$$= \frac{1}{2} \int \sigma_{ij} \epsilon_{ij} dV$$

Energy Density in
Elastic Medium

$$= \frac{1}{2} \sigma_{ij} \epsilon_{ij} = \frac{1}{2} C_{ijkl} \epsilon_{ij} \epsilon_{kl}$$

If we treat this as the definition of C_{ijkl} ,
then we see that we can assume the ~~tensor~~
of elasticity has another symmetry

$$C_{ijkl} = C_{klij}$$

which Elnore & Heald call the reciprocity relation.

Isotropic Solids

You'll show (7.4.2) explicitly that there are only two independent elastic constants for isotropic materials. It turns out we can write C_{ijkl} in terms of the identity tensor (Kronecker delta) δ_{ij} :

$$C_{ijkl} = 2\mu (\delta_{ik}\delta_{jl} + \delta_{il}\delta_{jk}) + \lambda \delta_{ij}\delta_{kl}$$

• Has all the symmetries $C_{ijkl} = C_{ijlk} = C_{jilk} = C_{klij}$

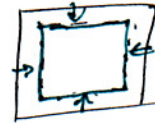
• Stress $\sigma_{ij} = C_{ijkl} \epsilon_{kl} = (2\mu (\delta_{ik}\delta_{jl} + \delta_{il}\delta_{jk}) + \lambda \delta_{ij}\delta_{kl}) \epsilon_{kl}$
set $k=i$
 $= 2\mu \epsilon_{ij} + \lambda \epsilon_{kk} \delta_{ij} = \frac{\nu}{1+\nu} \epsilon_{ij} + \frac{\nu \sigma}{(1+\nu)(1-2\nu)} \epsilon_{kk} \delta_{ij}$

• Energy = $\frac{1}{2} \sigma_{ij} \epsilon_{ij}$

$$= \mu \epsilon_{ij} \epsilon_{ij} + \frac{1}{2} \lambda (\epsilon_{kk})^2$$

Relation to Other Elastic Constants

Bulk Compression $P = -K \frac{\Delta V}{V}$



$$\frac{\Delta V}{V} = \frac{(L + \Delta L)^3 - L^3}{L^3} \approx \frac{3\Delta L}{L}$$

$$\epsilon_{ij} = \frac{\Delta L}{L} \delta_{ij} = \begin{pmatrix} \frac{\Delta L}{L} & 0 & 0 \\ 0 & \frac{\Delta L}{L} & 0 \\ 0 & 0 & \frac{\Delta L}{L} \end{pmatrix}$$

$$\sigma_{ij} = C_{ijkl} \epsilon_{kl}$$

$$= 2\mu \epsilon_{ij} + \lambda \epsilon_{kk} \delta_{ij} = 2\mu \frac{\Delta L}{L} \delta_{ij} + \lambda \left(\frac{3\Delta L}{L}\right) \delta_{ij}$$

$$= (2\mu + 3\lambda) \frac{\Delta L}{L} \delta_{ij} = \left(\frac{2\mu}{3} + \lambda\right) \frac{\Delta V}{V} \delta_{ij}$$

Hydrostatic Pressure: $\sigma_{ij} = -P \delta_{ij}$

$$P = -\left(\frac{2\mu}{3} + \lambda\right) \frac{\Delta V}{V}$$

$$K = \frac{2\mu}{3} + \lambda$$

Shear:



$$\partial_y u_x = \theta$$

Its Energy = $\frac{1}{2} \mu \theta^2$?

$$\epsilon_{ij} = \begin{pmatrix} 0 & \theta/2 & 0 \\ \theta/2 & 0 & 0 \\ 0 & 0 & 0 \end{pmatrix}$$

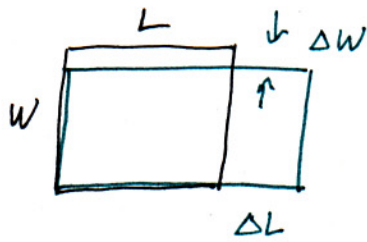
$$E = \mu \epsilon_{ij}^2 + \frac{\lambda}{2} \epsilon_{ii}^2 = \mu \sum_i \sum_j \epsilon_{ij} \epsilon_{ij} + \frac{\lambda}{2} \left(\sum_i \epsilon_{ii}\right) \left(\sum_j \epsilon_{jj}\right)$$

$$= \mu \left(\left(\frac{\theta}{2}\right)^2 + \left(\frac{\theta}{2}\right)^2 \right)$$

$$= \frac{1}{2} \mu \theta^2$$

$$\text{Shear Modulus} = \mu$$

Stretching (Unconstrained)



Needed:

- Stretch $\Delta L/L = a$
- Shrink $b = \frac{\Delta w}{w} = \frac{\Delta H}{H}$

to minimize energy density

- $b = \sigma a$
- $E = \frac{1}{2} Y a^2$

$$\epsilon_{ij} = \begin{pmatrix} \Delta L/L & 0 & 0 \\ 0 & -\frac{\Delta w}{w} & 0 \\ 0 & 0 & -\frac{\Delta w}{w} \end{pmatrix} = \begin{pmatrix} a & 0 & 0 \\ 0 & -b & 0 \\ 0 & 0 & -b \end{pmatrix}$$

$$\text{Energy density} = \mu \epsilon_{ij}^2 + \lambda/2 \epsilon_{ii}^2$$

$$= \mu \sum_i \sum_j \epsilon_{ij} \epsilon_{ij} + \frac{\lambda}{2} (\sum_i \epsilon_{ii}) (\sum_j \epsilon_{jj})$$

$$= \mu (a^2 + 2b^2) + \frac{\lambda}{2} (a - 2b)^2$$

$$= (\mu + \frac{\lambda}{2}) a^2 + (2\mu + 2\lambda) b^2 + 2\lambda ab$$

$$\frac{\partial \text{Energy}}{\partial b} = 4(\mu + \lambda) b - 2\lambda a = 0 \Rightarrow b = \frac{2\lambda}{4(\mu + \lambda)} a$$

$$\sigma = \frac{\lambda}{2(\mu + \lambda)}$$

$$\dots E = \frac{1}{2} \left(\frac{2\mu^2 + 3\lambda\mu}{\mu + \lambda} \right) a^2$$

$$Y = \frac{2\mu^2 + 3\lambda\mu}{\mu + \lambda}$$